

Task-Space Inverse Dynamics

Optimization-based Robot Control

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From Joint Space to Task Space Control

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What if we have reference trajectory $x^r(t)$ for **end-effector**?

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Tracking $q^r(t)$ is **sufficient but not necessary** to track $x^r(t)$: controller rejects also perturbations affecting q without affecting $FG(q)$.

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Finally compute joint torques as:

$$\tau = M\dot{\nu}^d + h \quad (5)$$

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Option 2 typically preferred:

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- More complex controller

End-effector control law (Option 2):

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End-Effector Control as LSP

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can be computed as:

$$\begin{aligned}\underset{\tau, \dot{v}}{\text{minimize}} \quad & \|J\dot{v} + \dot{J}v - \dot{v}^d\|^2 \\ \text{subject to} \quad & M\dot{v} + h = \tau\end{aligned}\tag{10}$$

Task Models

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N.B.

Here: e depends on instantaneous state-control value.

In **optimal control**: e depends on state-control trajectory.

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Solution

Impose dynamics of $e(x, t)$ (e.g., $\dot{e} = \dots$)

which should be affine function of \dot{v}

such that $\lim_{t \rightarrow \infty} e(x, t) = 0$

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End up with **affine** function of \dot{v} and u :

$$g(y) \triangleq \underbrace{\begin{bmatrix} A_v & A_u \end{bmatrix}}_A \underbrace{\begin{bmatrix} \dot{v} \\ u \end{bmatrix}}_y - a$$

Optimization-Based Control

Task-Space Inverse Dynamics (TSID)

Find τ that minimizes task function:

$$\begin{aligned} & \underset{y=(\dot{v}, \tau)}{\text{minimize}} && \|Ay - a\|^2 \\ & \text{subject to} && \begin{bmatrix} M & -S^\top \end{bmatrix} y = -h \end{aligned} \tag{13}$$

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If contacts are **soft**, use estimated forces \hat{f} :

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TSID for Robots in Rigid Contact

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Introduce forces and constraints:

$$\begin{aligned} & \underset{y=(\dot{v}, f, \tau)}{\text{minimize}} \quad \|Ay - a\|^2 \\ & \text{subject to} \quad \begin{bmatrix} J & 0 & 0 \\ M & -J^\top & -S^\top \end{bmatrix} y = \begin{bmatrix} -jv \\ -h \end{bmatrix} \end{aligned} \quad (15)$$

Inequality Constraints

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Any inequality **affine** in $y = (\tau, f, \dot{v})$:

- joint torque bounds: $\tau^{min} \leq \tau \leq \tau^{max}$
- (linearized) force friction cones: $Bf \leq 0$
- joint bounds: $\dot{v}^{min} \leq \dot{v} \leq \dot{v}^{max}$
- collision avoidance (more complicated)

Multi-Task Control

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Multi-Objective Optimization

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Can use redundancy to execute **secondary** tasks, but how?

Weighted Multi-Objective Optimization

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CONS Hard to find weights \rightarrow too large/small weights lead to **numerical issues**.

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- $n_v + n_{va} + n_f$ variables (≈ 70 for humanoid)
- $n_v + n_f$ equality constraints (≈ 40 for humanoid)
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QUESTIONS

- Can we solve it in 1 ms?
- Can we speed up computation?

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Identity matrix is easy to invert \rightarrow Easy to express τ as affine function of other variables.

$$\underbrace{\begin{bmatrix} \dot{v} \\ f \\ \tau \end{bmatrix}}_y = \underbrace{\begin{bmatrix} I & 0 \\ 0 & I \\ M_a & -J_a^\top \end{bmatrix}}_D \underbrace{\begin{bmatrix} \dot{v} \\ f \end{bmatrix}}_{\bar{y}} + \underbrace{\begin{bmatrix} 0 \\ 0 \\ h_a \end{bmatrix}}_d$$

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$$\underset{y}{\text{minimize}} \quad \|Ay - a\|^2$$

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Removed n_{va} variables and n_{va} equality constraints!

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BUT these tricks either limit expressiveness, or lead to small improvements (while making software more complex).

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BUT these tricks either limit expressiveness, or lead to small improvements (while making software more complex).

My opinion: not worth it!

So far $y(x, u) \in \mathbb{R}^m$.

From Euclidian Spaces to Lie Groups

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SOLUTION Represent $SE(3)$ elements using homogeneous matrices $y \in \mathbb{R}^{4 \times 4}$ and redefine error function:

$$e(q, t) = \log(y^*(t)^{-1}y(q)),$$

where $\log \triangleq$ inverse operation of matrix exponential (i.e. exponential map): transforms displacement into twist.

-  A. Del Prete, N. Mansard, F. Nori, G. Metta, and L. Natale.
Partial Force Control of Constrained Floating-Base Robots.
In *Intelligent Robots and Systems (IROS 2014), IEEE International Conference on*, 2014.
-  A. Herzog, N. Rotella, S. Mason, F. Grimminger, S. Schaal, and L. Righetti.
Momentum control with hierarchical inverse dynamics on a torque-controlled humanoid.
Autonomous Robots, 40(3):473–491, 2016.
-  M. Mistry, J. Buchli, and S. Schaal.
Inverse dynamics control of floating base systems using orthogonal decomposition.
2010 IEEE International Conference on Robotics and Automation, (3):3406–3412, may 2010.



L. Righetti, J. Buchli, M. Mistry, and S. Schaal.

Inverse dynamics control of floating-base robots with external constraints: A unified view.

2011 IEEE International Conference on Robotics and Automation,
pages 1085–1090, may 2011.